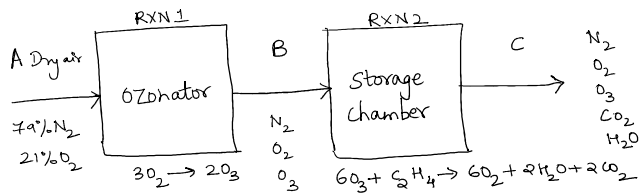


Question 14 : Incomplete Conversion of Ethylene



Let's start with a basis for dry air, $\dot{n}_{DA} = 100 \text{ mol air/h}$ in stream A

Balances around the ozonator,

N_2 : $ACC = IN - OUT + GEN$
 $0 = 79 \text{ mol/h} - \dot{n}_N^B + 0$
 $\dot{n}_N^B = 79 \text{ mol } N_2/\text{h}$

O_2 : $ACC = IN - OUT + GEN$
 $0 = 21 \text{ mol/h} - \dot{n}_{O_2}^B - \dot{n}_{O_2}^{RXN1} \quad (1)$
 $\text{Conversion} = \frac{\text{mol } O_2 \text{ consumed}}{\text{mol } O_2 \text{ fed}}$
 $0.07 = \frac{\dot{n}_{O_2}^{RXN1}}{21}$
 $\dot{n}_{O_2}^{RXN1} = 1.47 \text{ mol } O_2/\text{h}$

from 1, $0 = 21 - \dot{n}_{O_2}^B - 1.47$
 $\dot{n}_{O_2}^B = 19.53 \text{ mol } O_2/\text{h}$

O_3 : $ACC = IN - OUT + GEN$
 $0 = 0 - \dot{n}_{O_3}^B + \dot{n}_{O_3}^{RXN1} \quad (2)$
 $\dot{n}_{O_3}^{RXN1} = \frac{2 \text{ mol } O_3 \text{ generated}}{3 \text{ mol } O_2 \text{ consumed}} \times 1.47 \text{ mol } O_2 \text{ consumed/h}$
 $\dot{n}_{O_3}^{RXN1} = 0.98 \text{ mol } O_3/\text{h}$

From 2, $0 = 0 - \dot{n}_{O_3}^B + 0.98 \rightarrow \dot{n}_{O_3}^B = 0.98 \text{ mol } O_3/\text{h}$

Balance around the storage chamber,

N_2 : $ACC = IN - OUT + GEN$
 $0 = 79 \text{ mol/h} - \dot{n}_N^C + 0$
 $\dot{n}_N^C = 79 \text{ mol } N_2/\text{h}$

O_3 : $ACC = IN - OUT + GEN$
 $0 = 0.98 \text{ mol/h} - \dot{n}_{O_3}^C - \dot{n}_{O_3}^{RXN2} \quad (3)$

Percentage excess of O_3 is 80%

$$XS = \frac{\text{mol } O_3 \text{ fed} - \text{mol } O_3 \text{ consumed}}{\text{mol } O_3 \text{ consumed}}$$

$$0.8 = \frac{0.98 \text{ mol/h} - \dot{n}_{O_2}^{RXN2}}{\dot{n}_{O_2}^{RXN2}}$$

$$\dot{n}_{O_2}^{RXN2} = 0.54 \text{ mol } O_3/\text{h}$$

From 3,

$$0 = 0.98 - \dot{n}_{O_2}^C - \dot{n}_{O_2}^{RXN2}$$

$$0 = 0.98 - \dot{n}_{O_2}^C - 0.54$$

$$\dot{n}_{O_2}^C = 0.44 \text{ mol } O_3/\text{h}$$

C_2H_4 : How much C_2H_4 can we remove?

$$= \frac{1 \text{ mol } C_2H_4 \text{ cons.}}{6 \text{ mol } O_3 \text{ cons.}} \times 0.54 \text{ mol } O_3 \text{ cons/h}$$

$$= \underline{0.09 \text{ mol } C_2H_4/\text{h}}$$

O_2 :

$$ACC = IN - OUT + GEN$$

$$0 = 19.53 \text{ mol/h} - \dot{n}_{O_2}^C + \dot{n}_{O_2}^{RXN2} \quad - (4)$$

$$\dot{n}_{O_2}^{RXN2} = \frac{6 \text{ mol } O_2 \text{ generated}}{6 \text{ mol } O_3 \text{ consumed}} \times 0.54 \text{ mol } O_3 \text{ cons/h}$$

$$\dot{n}_{O_2}^{RXN2} = 0.54 \text{ mol } O_2/\text{h}$$

From 4,

$$0 = 19.53 - \dot{n}_{O_2}^C + 0.54$$

$$\dot{n}_{O_2}^C = 20.07 \text{ mol } O_2/\text{h}$$

CO_2 :

$$ACC = IN - OUT + GEN$$

$$0 = 0 - \dot{n}_{CO_2}^C + \dot{n}_{CO_2}^{RXN2} \quad - (5)$$

CO_2

$\dot{n}_{CO_2}^{RXN2}$

$$0 = 0 - \dot{n}_{CD}^c + \dot{n}_{CD} - (5)$$

$$\dot{n}_{CD}^{RXN2} = \frac{2 \text{ mol CO}_2 \text{ gen}}{6 \text{ mol O}_3 \text{ cons}} \times 0.54 \text{ mol O}_3 \text{ cons/h}$$

$$\dot{n}_{CD}^{RXN2} = 0.18 \text{ mol CO}_2/\text{h}$$

from 5, $0 = 0 - \dot{n}_{CD}^c + 0.18 \text{ mol/h}$

$$\dot{n}_{CD}^c = 0.18 \text{ mol CO}_2/\text{h}$$

H₂O:

$$ACC = IN - OUT + GEN$$

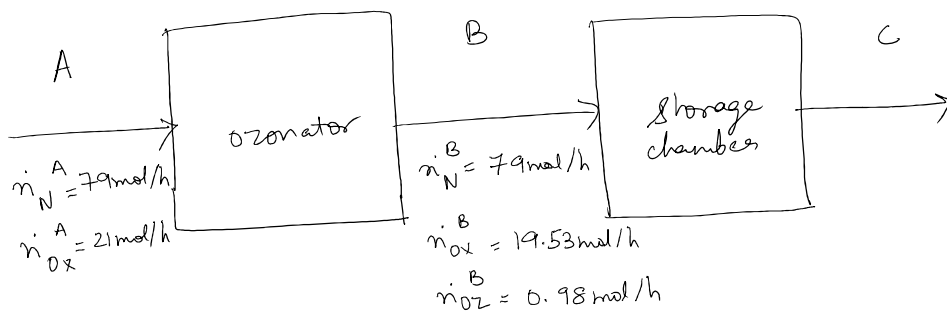
$$0 = 0 - \dot{n}_W^c + \dot{n}_W^{RXN2} - (6)$$

$$\dot{n}_W^{RXN2} = \frac{2 \text{ mol H}_2\text{O gen}}{6 \text{ mol O}_3 \text{ cons}} \times 0.54 \text{ mol O}_3/\text{h}$$

$$\dot{n}_W^{RXN2} = 0.18 \text{ mol H}_2\text{O/h}$$

from 6, $0 = 0 - \dot{n}_W^c + 0.18 \text{ mol/h}$

$$\dot{n}_W^c = 0.18 \text{ mol/h}$$



Summary of gases out in stream C,

	$\dot{n}_i (\text{mol/h})$	x_i
N ₂	79	0.79
O ₂	20.07	0.201

O_2	20.07	0.201
O_3	0.44	0.0044
CO_2	0.18	0.0018
H_2O	0.18	0.0018
Total $\rightarrow$	99.87	

Scale $\rightarrow$ for $n_{DA}^A = 100 \text{ mol/h}$, $0.09 \text{ mol } C_2H_4/h$ is removed.

$$\Rightarrow 16 \text{ tons of apples} \times \frac{6.5 \text{ g } C_2H_4}{\text{ton} \cdot h} \times \frac{\text{mol}}{28.05 \text{ g}} = \underline{3.71 \text{ mol } C_2H_4/h}$$

which means our basis of 100 mol/h is $3.71/0.09 \rightarrow 41.2$ times too small.

(i) Quantity of ozone generated:

$$n_{O_3}^B = 0.98 \text{ mol/h}$$

$$\Rightarrow \left(0.98 \frac{\text{mol } O_3}{h}\right) (41.2) = 40.4 \text{ mol } O_3/h \text{ or}$$

$$\left(40.4 \frac{\text{mol } O_3}{h}\right) \left(\frac{48 \text{ g } O_3}{1 \text{ mol } O_3}\right) = \underline{1.94 \text{ kg } O_3/h}$$

(ii) Quantity of dry air ^{to be} supplied to the ozonator:-

$$n_{DA}^A = 100 \text{ mol DA/h}$$

$$\Rightarrow \left(\frac{100 \text{ mol DA}}{h}\right) (41.2) = \underline{4120 \text{ mol DA/h}}$$

$$\Rightarrow \left(\frac{4120 \text{ mol DA}}{h}\right) \left(\frac{29 \text{ g DA}}{1 \text{ mol DA}}\right) = \underline{119.5 \text{ kg DA/h}}$$

(101.4 m³ DA/h at 25°C)

(iii) Composition of the exit gas (mole fraction calculated above)

$$\text{Total flow out} = \left(\frac{99.87 \text{ mol}}{h}\right) (41.2) = \underline{4115 \text{ mol/h}}$$